

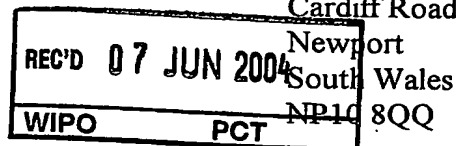


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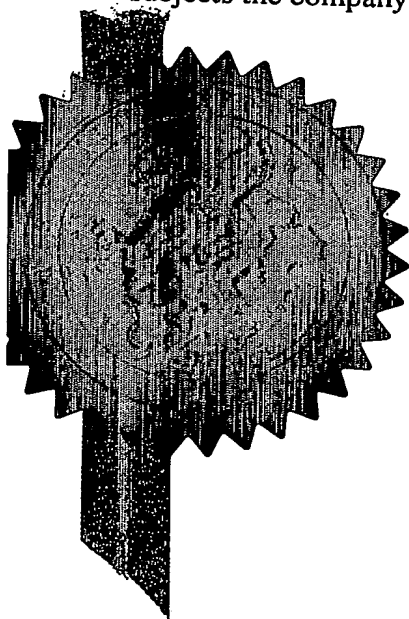


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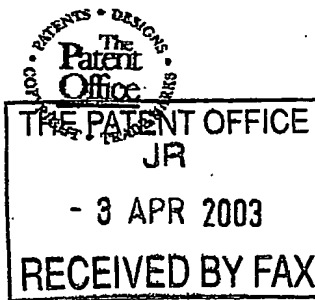
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# 1/77

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### 2. Patent application number

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0307724.5

sps.2843.uk.dkach  
03APR03 E797582-1 010002  
P01/7700 0.00-0307724.5

### 3. Full name, address and postcode of the or of each applicant (underline all surnames)

Specialised Petroleum Services Group Limited  
Wellbore Completion Services  
Arnhall Business Park  
Westhill  
ABERDEEN  
AB32 6TQ

Patents ADP number (if you know it)

If the applicant is a corporate body, give the country/state of its incorporation

United Kingdom

- 8460784001

### 4. Title of the invention

Improved Mechanism for Actuation of a Downhole Tool

### 5. Name of your agent (if you have one)

"Address for service" in the United Kingdom to which all correspondence should be sent (including the postcode)

Kennedys Patent Agency Limited  
Queens House, Floor 5  
29 St Vincent Place  
GLASGOW  
G1 2DT

Patents ADP number (if you know it)

08058240002

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Country

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Number of earlier application

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12. Name and daytime telephone number of person to contact in the United Kingdom

David Kennedy - 0141 226 6826

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1 Improved Mechanism for Actuation of a Downhole Tool

2

3 The present invention relates to downhole tools as used  
4 in the oil and gas industry and in particular, though not  
5 exclusively, to a mechanism for moving a sleeve in a  
6 downhole tool by passing a ball along a helical groove in  
7 the sleeve.

8

9 While many downhole tools operate continuously through a  
10 well bore e.g. scrapers and brushes as disclosed in US  
11 6,227,291, it is more desirable to provide a tool which  
12 performs a function only when it has reached a preferred  
13 location within a well bore. An example of such a tool  
14 would be a circulation tool as disclosed in WO 02/061236.  
15 The tool provides a cleaning action on the walls of the  
16 casing or lining of the well bore. The cleaning action is  
17 only required after the casing has been brushed or  
18 scraped and thus the tool is designed to be selectively  
19 actuated in the well bore. Such tools provide the  
20 advantage of allowing an operator to mount a number of  
21 tools on a single work string and operate them  
22 individually on a single trip in to the well bore. This  
23 saves significant time in making the well operational.

1 Tools which are selectively actuatable in a well bore  
2 commonly operate by having an element which can be moved  
3 relative to the tool when in the well bore. In the  
4 circulation tool of WO 02/061236, the element is a sleeve  
5 located in the cylindrical body of the tool. When run in  
6 the well, the sleeve is held in a first position by one  
7 or more shear screws. To actuate the tool, a drop ball  
8 is released from the surface of the well through the work  
9 string. On reaching the sleeve, the ball blocks the flow  
10 of fluid through the tool and consequently pressure  
11 builds up until the shear screws shear and the sleeve is  
12 forced downwards. The movement of the sleeve is then  
13 stopped when a lower ledge of the sleeve contacts a  
14 shoulder on the internal surface of the tool body.

15  
16 Such tools have a number of disadvantages. The tools are  
17 generally limited to one actuatable movement. If two  
18 sleeves are incorporated to overcome this, the shear  
19 screws of the second sleeve can operate prematurely under  
20 the shock created to shear the shear screws of the first  
21 sleeve. Additionally, the reduced bore diameter of the  
22 lower part also effects the flow rate achievable through  
23 the tool.

24  
25 One tool which has been developed to operate repeatedly  
26 is that disclosed in US 4,889,199. This tool comprises a  
27 tubular body having a radial port into which is located a  
28 sleeve having a matching radial port. The sleeve is  
29 slidably mounted and its action controlled from a  
30 deformable drop ball biasing the sleeve against a spring.  
31 Initially the spring biases the sleeve to a closed  
32 position in which the ports are misaligned. The drop ball  
33 causes the sleeve to move to a position where the ports

1 align due to a build up of pressure behind the ball, and  
2 fluid is discharged radially through the ports. A small  
3 steel ball is then dropped into the tool which seals the  
4 radial ports and the consequential pressure build up  
5 extrudes the deformable ball through the ball seat. The  
6 steel ball will drop with the deformable ball and both  
7 are retained in a ball catcher at the base of the tool.  
8 When the balls drop together the spring biases the sleeve  
9 back to the closed position and the tool can be operated  
10 repeatedly.

11  
12 A disadvantage of this tool is that it requires both a  
13 deformable ball and a smaller metal ball to operate. Care  
14 must then be taken to ensure the balls are dropped in the  
15 correct order. The smaller metal ball must lodge in the  
16 second, radial, outlet in order to stop flow and thus the  
17 tool is restricted to having a single radial port. This  
18 limits the amount of cleaning which can be performed. Yet  
19 further is a disadvantage in that use of a rubber or  
20 deformable ball is unreliable as the material can break  
21 up or wear within the well bore.

22  
23 It is an object of the present invention to provide an  
24 actuation mechanism for a downhole tool which obviates or  
25 mitigates at least some of the disadvantages of the prior  
26 art.

27  
28 It is a further object of at least one embodiment of the  
29 present invention to provide an actuation mechanism to  
30 move a sleeve within a downhole tool.

31  
32 It is a yet further object of at least one embodiment of  
33 the present invention to provide an actuation mechanism

1 for use in a downhole tool which is re-settable to allow  
2 the tool to operate in a cyclic manner.

3

4 It is yet further object of at least one embodiment of  
5 the present invention to provide a circulation tool which  
6 can be operated repeatedly using a single ball.

7

8 According to a first aspect of the present invention  
9 there is provided an actuation mechanism for a downhole  
10 tool, the mechanism comprising a substantially  
11 cylindrical body having a central bore running axially  
12 therethrough, a sleeve located within the bore, the  
13 sleeve including a helical channel on an inner surface,  
14 mechanical biasing means located between the sleeve and  
15 the body to bias the sleeve in a first direction and a  
16 ball, sized to run in the helical channel in a reverse  
17 direction to prevent a majority of fluid flow through the  
18 sleeve and cause the sleeve to move in the reverse  
19 direction relative to the body.

20

21 When the ball is dropped in the body, fluid will drive  
22 the ball into the channel and into the helical path. As  
23 the ball is sized for the channel it will block the  
24 majority of the fluid path through the tool and  
25 consequently pressure will build up on the ball. This  
26 pressure will be sufficient to move the ball and sleeve  
27 together against the spring and force the sleeve in the  
28 reverse direction. The movement of the sleeve actuates  
29 the tool. On release of the ball from the channel the  
30 sleeve is biased in the first direction back to its  
31 original position.

32

1 Preferably the mechanical bias is a strong spring. The  
2 spring may be helical, conical or the like. A strong  
3 string will prevent the sleeve moving in the reverse  
4 direction by fluid flow in the central bore.

5  
6 Preferably the helical channel has curved walls. This  
7 will prevent damage to the ball. Preferably also the ball  
8 is sized to provide a fluid by-pass around the ball when  
9 in the channel. This ensures a positive pressure is  
10 maintained behind the ball and prevents chattering of the  
11 ball in the channel.

12  
13 The helical channel may be considered as a screw thread.  
14 Thus the channel has a left hand thread so that the ball  
15 travels in the opposite direction to the rotation of the  
16 tool on a work string. Preferably a pitch of the thread  
17 is greater than or equal to a diameter of the ball.

18  
19 Preferably the ball is spherical. More preferably the  
20 ball is of a non-pliable material and thus cannot deform.  
21 Advantageously the ball is made of steel.

22  
23 Preferably also the sleeve includes a conical surface at  
24 an entrance to the channel. This funnels the ball into  
25 the channel and ensures it travels into the helical path.

26  
27 According to a second aspect of the present invention  
28 there is provided a downhole tool for circulating fluid  
29 in a borehole, the tool comprising a substantially  
30 cylindrical body having a central bore running axially  
31 therethrough, the body including at least one first port  
32 arranged substantially transversely to the central bore,  
33 a sleeve located within the bore, the sleeve including at



1 least one second port arranged transversely to the  
2 central bore for discharging fluid from the central bore  
3 when the first and second ports are aligned and  
4 mechanical biasing means located between the sleeve and  
5 the body to bias the sleeve in a first direction at which  
6 the ports are misaligned, wherein at least a portion of  
7 the sleeve includes a helical channel on an inner surface  
8 thereof, and the tool further includes at least one ball,  
9 the ball being sized to run in the helical channel in a  
10 reverse direction to prevent a majority of fluid flow  
11 through the sleeve and cause the sleeve to move in the  
12 reverse direction relative to the body so that the ports  
13 come into alignment.

14  
15 Preferably the mechanical bias is a strong spring. The  
16 spring may be helical, conical or the like. A strong  
17 string will prevent the sleeve moving in the reverse  
18 direction by fluid flow in the central bore.

19  
20 Preferably the helical channel has curved walls. This  
21 will prevent damage to the ball. Preferably also the ball  
22 is sized to provide a fluid by-pass around the ball when  
23 in the channel. This ensures a positive pressure is  
24 maintained behind the ball and prevents chattering of the  
25 ball in the channel.

26  
27 The helical channel may be considered as a screw thread.  
28 Thus the channel has a left hand thread so that the ball  
29 travels in the opposite direction to the rotation of the  
30 tool on a work string. Preferably a pitch of the thread  
31 is greater than or equal to a diameter of the ball.

32

1 Preferably the ball is spherical. More preferably the  
2 ball is of a non-pliable material and thus cannot deform.  
3 Advantageously the ball is made of steel.  
4

5 Preferably also the sleeve includes a conical surface at  
6 an entrance to the channel. This funnels the ball into  
7 the channel and ensures it travels into the helical path.  
8

9 Preferably the tool further comprises engagement means to  
10 control relative movement between the sleeve means and  
11 the body. Preferably also the mechanical bias biases the  
12 sleeve against the engagement means.  
13

14 Preferably also the tool includes ball collecting means.  
15 The ball collecting means may be an element located in  
16 the casing means to prevent passage of the ball through  
17 the tool, but allowing passage of fluid through the tool.  
18

19 Preferably said first and second ports are located  
20 substantially perpendicular to a longitudinal axis  
21 through the tool. More preferably there are a plurality  
22 of said first and said second ports. Advantageously there  
23 are three or more said first and said second outlets.  
24 Preferably also said first and said second outlets are  
25 spaced equidistantly around the body and the sleeve  
26 respectively.  
27

28 Preferably said engagement means comprises at least one  
29 index pin located in a profiled groove. Preferably the at  
30 least one index pin is located on the body and the  
31 profiled groove is located on an outer surface of the  
32 sleeve. In this way, an index sleeve is produced with the  
33 groove determining the relative position of the sleeve to

1 the body. Advantageously the groove extends  
2 circumferentially around the sleeve, thus the tool can be  
3 continuously cycled.

4

5 Preferably also the spring is located in a chamber  
6 created between the sleeve and the body. Advantageously  
7 the chamber includes an exhaust port such that fluid can  
8 enter and be dispelled from the chamber by relative  
9 movement of the sleeve and the body.

10

11 According to a third aspect of the present there is  
12 provided a method of actuating a tool in a borehole, the  
13 method comprising the steps;

14

- 15 (a) inserting in a work string a tool including an  
16 actuating mechanism according to the first aspect;  
17 (b) running the work string and tool into a borehole,  
18 with the tool in a first operating position;  
19 (c) dropping a ball into the work string such that the  
20 ball travels along the helical channel and by virtue  
21 of an increase in pressure on the ball, forcing the  
22 sleeve to move and switching the tool to a second  
23 operating position; and  
24 (d) on exit of the ball from the channel, returning the  
25 tool to the first operating position as the  
26 mechanical bias acts on the sleeve.

27

28 According to a fourth aspect of the present invention  
29 there is provided a method of circulating fluid in a  
30 borehole, the method comprising the steps:

31

32

- 1 (a) inserting in a work string a tool including an
- 2 actuating mechanism according to the second aspect;
- 3 (b) running the work string and tool into a borehole,
- 4 with the tool in a closed position wherein the ports
- 5 are misaligned and fluid flows through the central
- 6 bore;
- 7 (c) dropping a ball into the work string such that the
- 8 ball travels along the helical channel and by virtue
- 9 of an increase in pressure on the ball, forcing the
- 10 sleeve to move and switching the tool to an open
- 11 position wherein the ports are aligned;
- 12 (d) discharging fluid from the ports; and
- 13 (e) on exit of the ball from the channel, returning the
- 14 tool to the closed position as the mechanical bias
- 15 acts on the sleeve.

16  
17 Preferably the method further includes the steps of:

- 18
- 19 (f) dropping a second ball, identical to the first ball,
- 20 into the work string such that the second ball
- 21 travels along the helical channel and by virtue of
- 22 an increase in pressure on the ball, forcing the
- 23 sleeve to move and switching the tool to an open
- 24 position wherein the ports are aligned;
- 25 (g) discharging fluid from the ports; and
- 26 (h) on exit of the ball from the channel, returning the
- 27 tool to the closed position as the mechanical bias
- 28 acts on the sleeve.

29  
30 With the sleeve and back in the first position, the steps

- 31 (f) to (h) can be repeated any number of times.

32

1 Preferably also the method includes the step of catching  
2 the dropped balls in the work string.

3

4 According to a fifth aspect of the present invention  
5 there is provided a method of circulating fluid in a  
6 borehole, the method comprising the steps:

7

- 8 (a) inserting in a work string a tool including an  
9 actuating mechanism according to the second aspect;  
10 (b) running the work string and tool into a borehole,  
11 with the tool in a first position wherein the ports  
12 are misaligned and fluid flows through the work  
13 string;  
14 (c) dropping a ball into the work string such that the  
15 ball travels along the helical channel and by virtue  
16 of an increase in pressure on the ball, forcing the  
17 sleeve to move into a second position relative to  
18 the body wherein the ports are misaligned and fluid  
19 flow is through the work string;  
20 (d) on exit of the ball from the channel, moving the  
21 tool to a third position by virtue of the mechanical  
22 bias acting on the sleeve wherein the ports are  
23 aligned and fluid flows through the ports.

24

25 Preferably the method further includes the steps of:

26

- 27 (e) dropping a second ball, identical to the first ball,  
28 into the work string such that the second ball  
29 travels along the helical channel and by virtue of  
30 an increase in pressure on the ball, forcing the  
31 sleeve to move the second position relative to the  
32 casing wherein the first and second ports are

1 misaligned and fluid flow is through the work  
2 string; and

3 (f) on exit of the ball from the channel, moving the  
4 sleeve to the first position by virtue of the  
5 mechanical wherein the first and second ports are  
6 misaligned and fluid flows through the work string.  
7

8 With the sleeve and casing back in the first position,  
9 the steps (c) to (f) can be repeated any number of times.  
10

11 Preferably also the method includes the step of catching  
12 the dropped balls in the work string.  
13

14 An embodiment of the present invention will now be  
15 described by way of example only with reference to the  
16 following Figures, of which:  
17

18 Figure 1 is a part cross-sectional view of a downhole  
19 tool in a first position according to an embodiment of  
20 the present invention;  
21

22 Figure 2 is a part cross-sectional view of the downhole  
23 tool of Figure 1 in a second position;  
24

25 Figure 3 is a part cross-sectional view of the downhole  
26 tool of Figure 1 in a third position; and  
27

28 Figures 4(a)-(c) are schematic illustrations of an index  
29 pin positioned in a groove of the tool of Figure 1 for  
30 the first, second and third positions respectively.  
31

32 Reference is initially made to Figure 1 of the drawings  
33 which illustrates a downhole tool, generally indicated by

1 reference numeral 10, in accordance with an embodiment of  
2 the present invention. Tool 10 includes a cylindrical  
3 body 12 having an upper end 14, a lower end 16 and a  
4 cylindrical bore 18 running therethrough. The body 12 has  
5 a box section 20 located at the upper end 14 and a pin  
6 section 22 located at the lower end 16 for connecting the  
7 tool 10 in a work string or drill string (not shown).

8  
9 The body 12 further includes four radial ports 24 located  
10 equidistantly around the body 12. The ports 24 are  
11 perpendicular to the bore 18.

12  
13 Located on an inner surface 26 of the body 12 are two  
14 opposing ledges 26, 28 used to limit axial movement of a  
15 sleeve 30 located within the body 12. Sleeve 30 is sealed  
16 against body 12 by o-rings 31a-d.

17  
18 Sleeve 30 is an annular body which also includes four  
19 radial ports 32 located equidistantly around the sleeve  
20 30. The ports 32 are perpendicular to the bore 18. The  
21 ports 32 are of a similar size to the ports 24 in the  
22 body 12.

23  
24 At an upper end 36 of the sleeve 30 is located a conical  
25 surface 38 facing the upper end 14 of the tool 10.  
26 Downwardly extending from the conical surface is a  
27 helical channel 34. The channel 34 comprises a continuous  
28 spiral groove, having curved walls 40, which takes the  
29 path of a screw thread on the inner surface 39 of the  
30 sleeve 30. The handedness of the 'screw thread' is left  
31 handed.

32

1 Located between the outer surface 44 of the sleeve 30 and  
2 the inner surface 46 of the body 12 is a space forming a  
3 chamber 48. The upper edge of the chamber is formed from  
4 a ledge 50 on the outer surface 44 of the sleeve 30. The  
5 lower edge of the chamber 48 is formed from the ledge 28  
6 of the body 12. A strong spring 52 is positioned within  
7 the chamber 48 and compressed to bias against the ledge  
8 50 of the sleeve 30. An exhaust port 54 is located  
9 through the sleeve 30 at the chamber 48 to allow fluid  
10 from the bore 42 to pass in to and out of the chamber 48  
11 as the sleeve 30 is moved relative to the body 12.  
12

13 Further an engagement mechanism, generally indicated by  
14 reference numeral 56, couples the sleeve 30 to the body  
15 12 and controls relative movement there between.  
16 Engagement mechanism 56 comprises an index sleeve 58,  
17 being a portion of the sleeve 30, and a matching index  
18 pin 60 located through the body 12 towards the sleeve 30.  
19 Index sleeve 58 includes a profiled groove 62 on the  
20 outer surface 44 of the sleeve 30 into which the index  
21 pin 60 locates.  
22

23 Reference is now made to Figure 4 of the drawings which  
24 illustrates the groove 62 of the index sleeve 58. The  
25 groove 62 extends circumferentially around the sleeve 30  
26 in a continuous path. The groove 62 defines a path having  
27 a substantially zig-zag profile to provided axial  
28 movement of the sleeve 30 relative to the body 12.  
29 Indeed, spring 52 biases the sleeve 30 against the index  
30 pin 60. The path includes an extended longitudinal  
31 portion 64 at every second upper apex of the zig-zag.  
32 Further a stop 66 is located at the apexes of the zig-  
33 zags to encourage the index pin 60 to remain at the



1 apexes and provide a locking function to the tool 10. The  
2 stops 66 are in the direction of travel of the pin 60  
3 along the groove 62.

4

5 Reference is now made to Figure 2 of the drawings which  
6 illustrates the tool 10 of Figure 1, now with a ball 68  
7 located in the bore 42. Like parts to those of Figure 1  
8 have been given the same reference numeral for ease of  
9 identification. Ball 68 is sized to travel along the  
10 helical channel 34. Ideally the ball 68 is sized to have  
11 a diameter less than or equal to the pitch of the screw  
12 thread forming the walls 40 of the channel 34. In this  
13 way when the ball 68 travels along the channel 34 a by-  
14 pass is created between the edge of the ball 68 and the  
15 walls 40 of the channel 34. The ball is of a hard  
16 material which is non-pliable. Ideally the ball is made  
17 of a metal such as steel.

18

19 Reference is now made to Figure 3 of the drawings which  
20 illustrates the tool 10 of Figure 1, now with the ball 68  
21 exiting the sleeve 30 into the bore 18. Like parts to  
22 those of Figures 1 and 2 have been given the same  
23 reference numeral for ease of identification. Body 12  
24 includes a pin 70 located into the bore 18. Pin 70 is a  
25 ball retainer pin which blocks the passage of the ball 68  
26 through the bore 18. Ball 68 will come to rest at the pin  
27 70 and therefore be retrievable with the tool 10. Pin 70  
28 does not prevent the flow of fluid through the bore 18  
29 and from the tool 10 into the work string below. The pin  
30 70 and the space 72 in the bore 18 immediately above it  
31 may be considered as a ball catcher.

32

1 In use, tool 10 is connected to a work string using the  
2 box section 20 and the pin section 22. As shown in  
3 Figures 1 and 4(a), the spring 52 biases the sleeve 30  
4 against the index pin 60 such that the pin 60 is located  
5 in the base apex of the groove 62. This is referred to as  
6 the first position of the tool 10. In this position,  
7 sleeve ports 32 are located above body ports 24, thus  
8 preventing fluid flow radially through these ports due to  
9 their misalignment. All fluid flow is through bores 18, 42  
10 of the tool 10. The tool 10 is then run into a bore hole  
11 until it reaches a location where cleaning of the bore  
12 hole casing or circulation of the fluid through the tool  
13 is required.

14

15 Drop ball 68 is then released through the bore of the  
16 work string from a surface. Ball 68 travels by fluid  
17 pressure to the conical surface 38 at the upper end 36 of  
18 the sleeve 30. The ball 68 is funnelled into the helical  
19 channel 34 where its progress is arrested. As the ball 68  
20 is now blocking the majority of fluid flow through the  
21 bore 42, fluid pressure will build up behind the ball and  
22 force the ball along the helical channel 34. Due to the  
23 size of the ball a small amount of fluid will be allowed  
24 to by-pass the ball 68. This fluid by-pass ensures that a  
25 positive pressure is maintained behind the ball 68 so  
26 that the ball 68 does not flow towards the upper end 14  
27 of the tool 10 also prevents the ball 68 from  
28 'chattering' in the channel 34. As the ball 68 makes its  
29 way along the channel 34 it acts as a temporary flow  
30 restrictor allowing sufficient pressure to build up on  
31 the ball 68 and sleeve 30 such that they can move in the  
32 direction of applied pressure against the bias of the  
33 spring. Consequently the sleeve 30 and ball 68 move to a

1 second position. This position is illustrated in Figure 2  
2 and 4(b). Though the ball 68 at the top of the channel 34  
3 it will be appreciated that this position can be reached  
4 with the ball in this position or when the ball 68 has  
5 travelled a distance down the channel 34. The spring 52  
6 is compressed into a now smaller chamber 48. Fluid has  
7 been expelled from the chamber 48 through the exhaust  
8 port 54. The index pin 60 is now located at the top of  
9 the longitudinal portion 64 of the groove 62.  
10 Consequently the sleeve ports 32 have crossed the body  
11 ports 24 and are now located below them. Fluid flow is  
12 thus still entirely through the bores 18,42.  
13  
14 On reaching the base of the channel 34, at the sleeve  
15 port 32, the ball 68 exits the channel 34 and free falls  
16 from this point. The ball 68 travels by fluid pressure  
17 until it is stopped by the pin 70 and is held in the  
18 space 72. On release of the pressure, spring 52 moves the  
19 sleeve 30 against the index pin 60 such that sleeve  
20 travels to a third position. The third position is  
21 illustrated in Figures 3 and 4(c). Fluid has been drawn  
22 into the chamber 48 and this drawing and expelling of  
23 fluid provides a hydraulic damping effect on the impact  
24 on the pin 60. Index pin 60 is now located in an upper  
25 apex of the groove 62 and the ports 24,32 are aligned. In  
26 this third position fluid is expelled radially from the  
27 tool 10 through the now aligned ports 24,32. The tool 10.  
28 is locked in this position by virtue of the stop 66 on  
29 the groove 62 which prevents movement of the sleeve 30  
30 for small variations in fluid pressure.  
31  
32 In order to close the ports 24,32, a second ball is  
33 dropped from the surface through the work string. The

1 second ball, and indeed any ball subsequent to this, is  
2 identical to the first ball 68. The second ball will  
3 travel to the conical surface 38. On the build up of  
4 fluid pressure behind the ball 68 it travels along the  
5 helical channel 34 and sleeve 30 will move downwards  
6 against the bias of the spring 52. Consequently the index  
7 pin 60 will be relocated into the next longitudinal  
8 groove 64 of the groove 62 and thus the tool is returned  
9 to the second position. When the second ball exits the  
10 helical channel 34, the pin 60 and sleeve 30 will move  
11 relatively back to the first position and the second ball  
12 will come to rest by the first ball 68. Effectively the  
13 tool is reset and by dropping further balls the tool 10  
14 can be repeatedly cycled in an open and closed manner as  
15 often as desired.

16  
17 It will be appreciated that although the description  
18 refers to relative positions as being 'above' and  
19 'below', the tool of the present invention can equally  
20 well be used in horizontal or inclined boreholes and is  
21 not restricted to vertical boreholes. Additionally the  
22 term 'borehole' can be used to refer to an open, cased or  
23 lined well bore.

24  
25 The principal advantage of the present invention is that  
26 it provides an actuating mechanism which can be  
27 repeatedly operated in a downhole tool. Further the  
28 mechanism dispenses with the need for a ball seat having  
29 a diameter smaller than the diameter of the drop ball and  
30 thus the flow through area of a tool incorporating the  
31 mechanism is improved over prior art drop ball actuated  
32 tools.

33

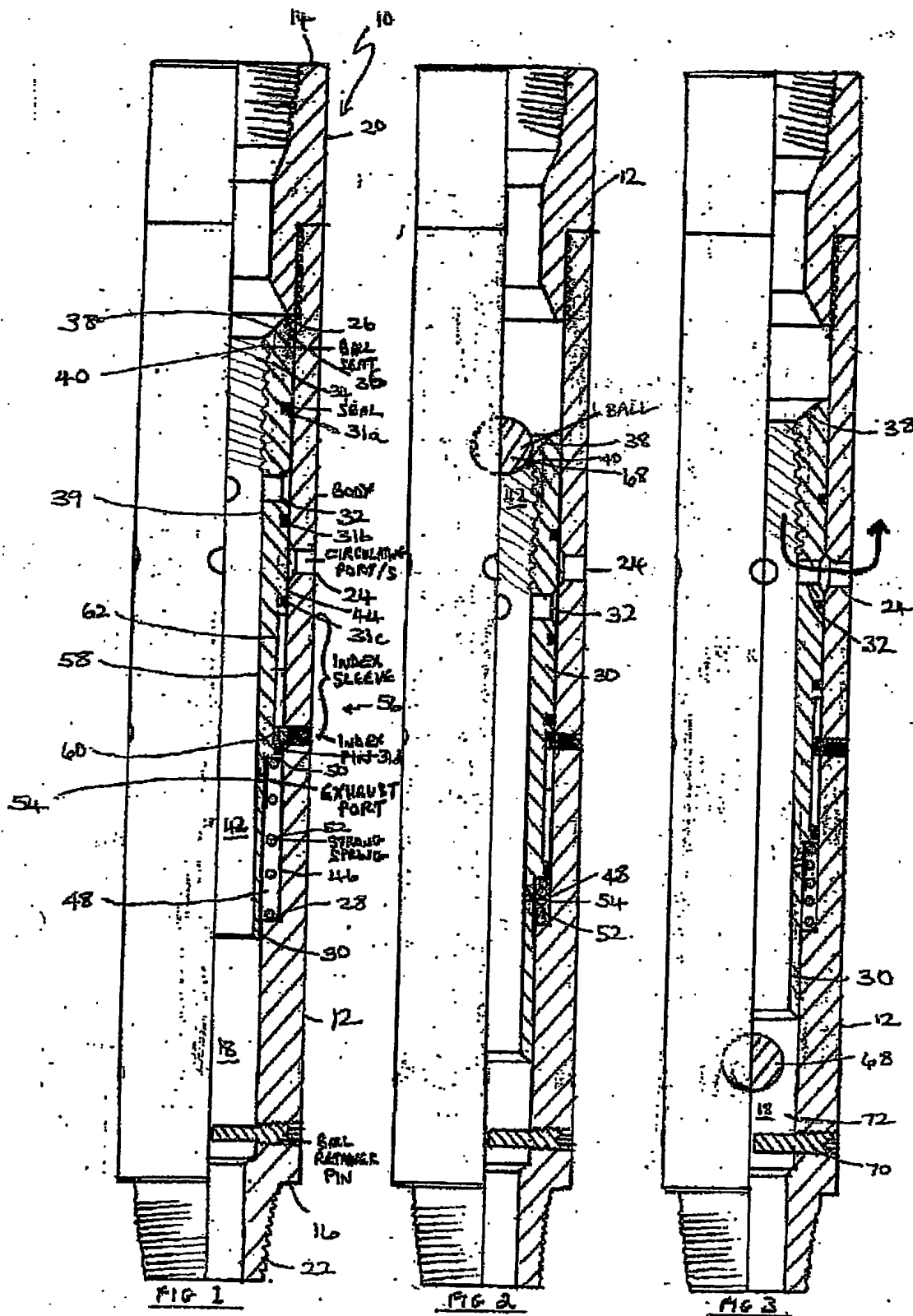
1 Further an embodiment of the invention advantageously  
2 provides a downhole tool for circulating fluid in a  
3 borehole which can be repeatedly operated by dropping  
4 identical balls through the work string. A further  
5 advantage is that the tool can have any number of radial  
6 ports to increase the flow area if desired compared with  
7 the prior art.

8  
9 Further as the actuating mechanism is located above the  
10 ports, the ports are opened with no flow going across the  
11 seals. This effectively saves the seals from excessive  
12 wear. An additional advantage is in the ability of the  
13 index sleeve to lock the circulating ports in position  
14 when aligned. Yet further the entry and exit of fluid in  
15 the chamber for the spring advantageously reduces the  
16 impact on the index pin via the hydraulic damping effect.

17  
18 Various modifications may be made to the invention herein  
19 described without departing from the scope thereof. For  
20 example, two or more index pins could be used to provide  
21 increased stability to the tool and distribute the load  
22 on the pins. Additional radial ports could be located at  
23 longitudinal spacings on the tool to provide radial fluid  
24 flow across a larger area when the ports are open. The  
25 ports may have varying diameters which may provide a  
26 nozzle on the outer surface of the body to increase fluid  
27 velocity.

28

1/2



2/2

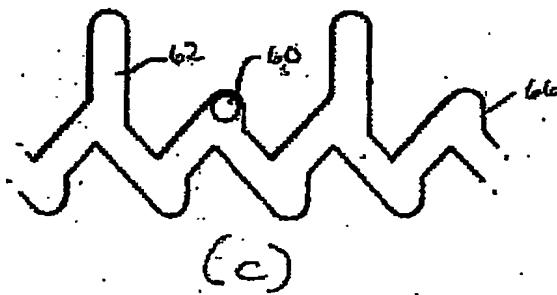
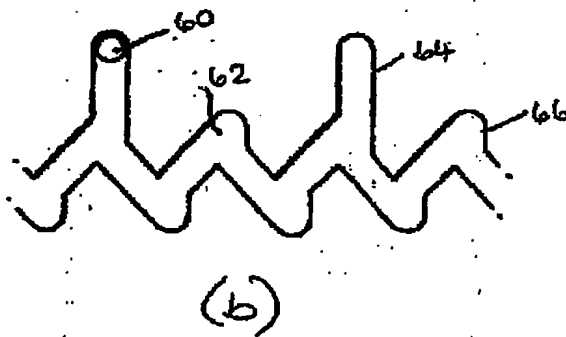
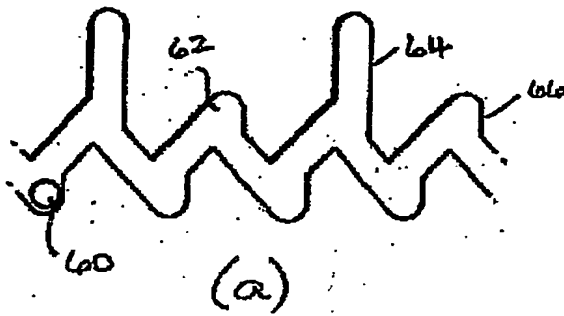


FIG 4

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